



# IMPACTS OF H<sub>2</sub>-ENRICHED NG FOR FEEDSTOCK OF LNG LIQUEFACTION

PHMSA LNG WORKSHOP NOVEMBER 15, 2022

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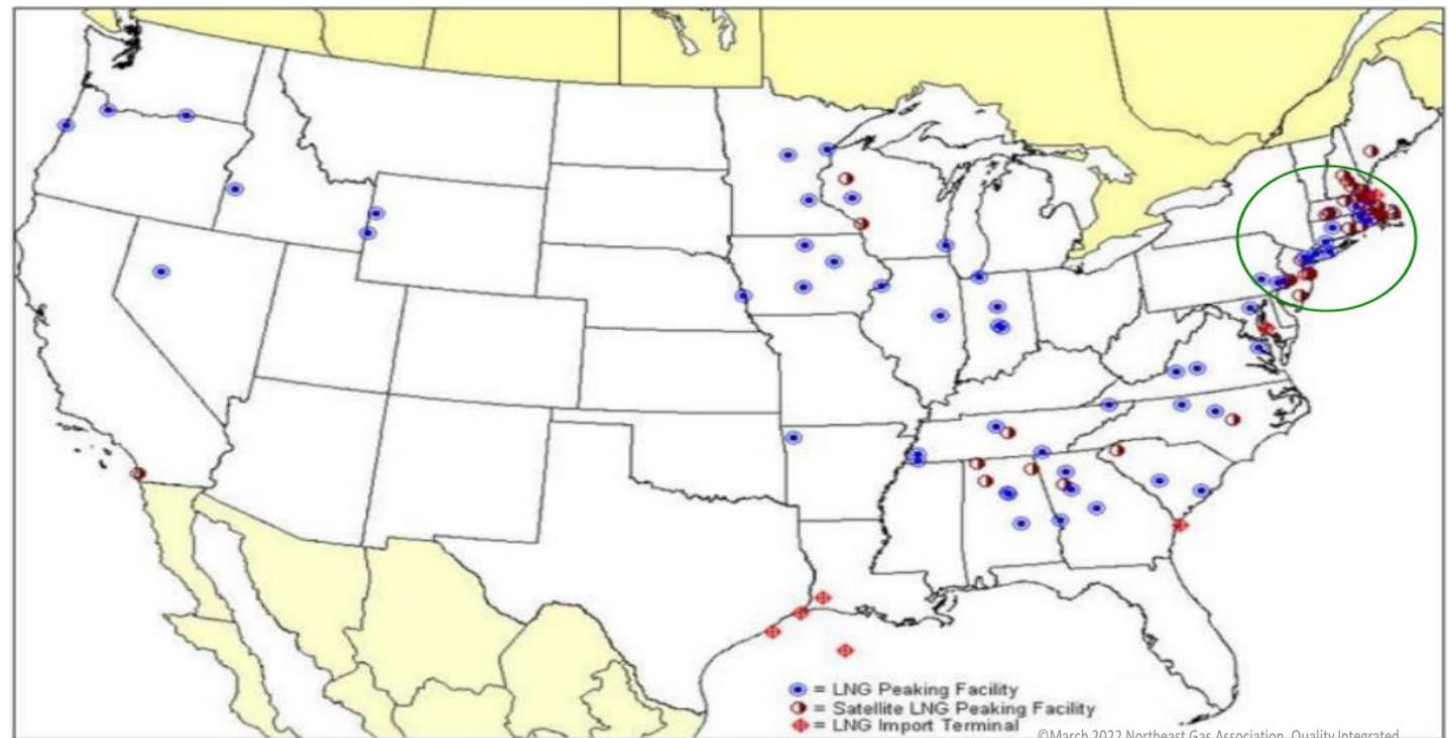
# NYSEARCH

- NYSEARCH is a sub-organization of NGA that conducts voluntary RD&D on behalf of 20+ utilities located in the United States and Canada
- Serving the gas utility industry by identifying and executing research programs to advance the safety, integrity, and efficiency of the gas utility
- Voluntary-based funding
- High leverage of R&D dollar
- Unique access to information on state-of-the-art technologies and research in an open setting with other gas utilities that experience similar, if not the same, challenges in operations



# BACKGROUND

- November 2021, NGA conducted an H2 Enriched NG Technical Workshop
  - NGA, AGA, NYSEARCH, and other companies who attended the workshop endorsed the idea to investigate the challenges and mitigation techniques should NG liquefaction pipelines include H2



Source: U.S. Energy Information Administration

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# NYSEARCH MULTI-PHASE PROGRAM

## Phase I: HENG LNG Feedstock Implications Study

- Develop an inventory of materials from the participating funders
- Detailed analysis of four participating funder facilities
- Identify any additional needs for further research

## Phase II: HENG Feedstock Pre- treatment Mitigation Measure Options to Enable Facility Operations

- Consider a range of pre-treatment, recovery, and reinjection options



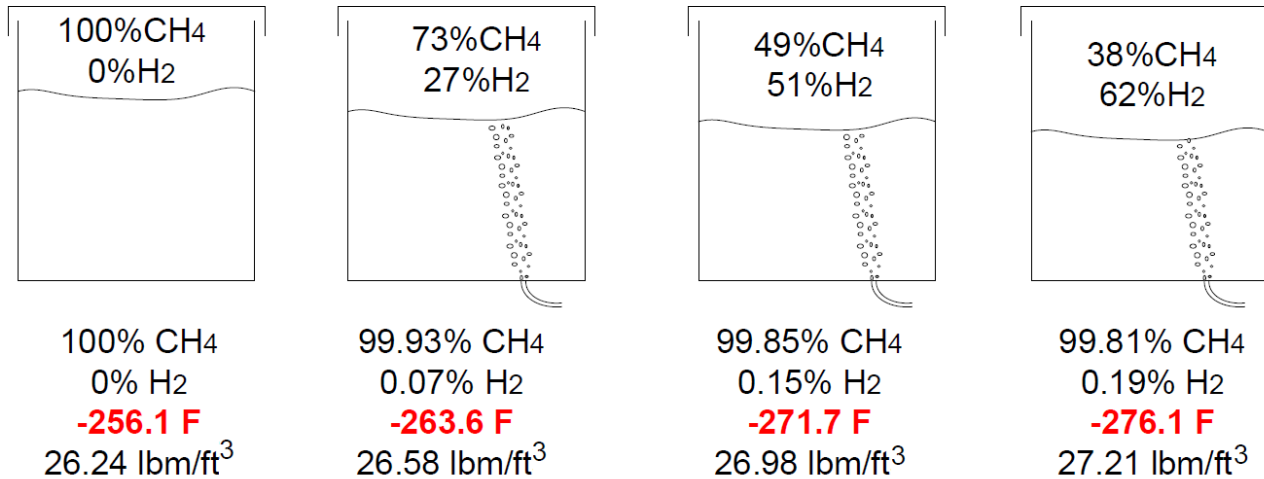
# THINGS ARE CHANGING IN OUR INDUSTRY

- The likelihood of Hydrogen Enriched Natural gas (HENG) coming into the natural gas system is high
- Hydrogen “for the most part” stays a vapor as it passes through a liquefaction plant, but it does behave oddly with phase changes related to pressure and temperature
- During the liquefaction process at higher pressures H<sub>2</sub> does see phase changes, which can significantly affect liquefaction capacity and ability to liquefy (CB&I article October 22 “LNG Industry”)
- Our findings involve the impact of very small concentrations of H<sub>2</sub> that does liquefy into the LNG inventory if not removed from the LHENG process
  - Hydrogen will most likely need to be removed from the feed gas before liquefaction (GasTech AP presentation 9/29/22)



# THERMODYNAMIC MODELS WITH LIQUID METHANE

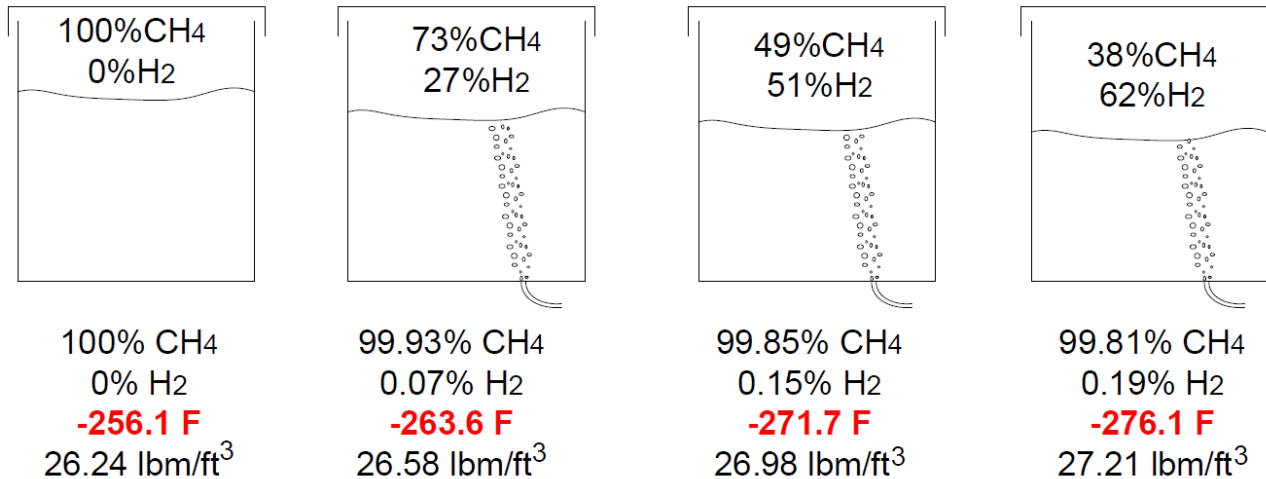
Well insulated tank at 16.5 psia and hydrogen bubbled through the liquid methane  
Using a combination of REFPROP and HYSYS data



- Consider what happens when we bubble pure hydrogen through an existing inventory of LM
- H<sub>2</sub> concentration dominates temperature and temperature (not H<sub>2</sub> concentration) dominates LM density

# HYDROGEN WITH LIQUID NATURAL GAS

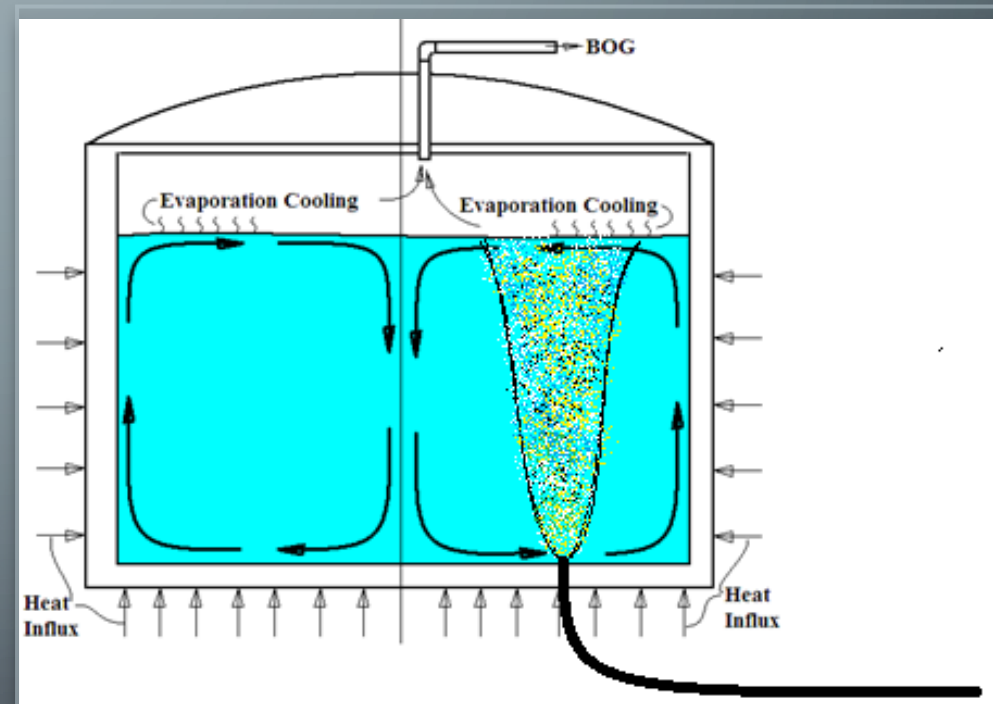
Well insulated tank at 16.5 psia and hydrogen bubbled through the liquid methane  
Using a combination of REFPROP and HYSYS data



- Consider what happens when we bubble pure hydrogen through an existing inventory of LNG
  - “Forced” additional CH<sub>4</sub> evaporation
- The methane vapor pressure above the liquid becomes much lower as hydrogen is added

# DENSITY OF THE LNG, STRATIFICATION, AND OUT-GASSING

- Indeterminant
  - When the bubbles are methane, they would condense in the subcooled LM at the bottom of the tank
  - When the bubbles are hydrogen, they do not condense but rise through the LM





ASSUME WE  
CAN GET THE  
LIQUEFIER TO  
MAKE COLD  
HENG BEFORE  
THE JT VALVE,  
THEN WHAT  
HAPPENS  
ACROSS THE JT  
VALVE?

- HYSYS was used to flash LM and LNG across a JT valve from 400 psia to tank pressure.
- We know LNG production would be reduced due to:
  - Reduced residence time in heat exchangers
  - Cooling of vapor that refuses to liquefy – that cold vapor enters and then leaves the tank
  - Heat transfer to a vapor is much less than to a liquid
- Presume these issues are overcome and we have the refrigerated Liq/Vap HENG upstream of the JT valve. What happens after the JT valve?

# HENG ACROSS A JT VALVE

Run Name	Stream 1					Stream 2					
	Psia	T (F)	Mth	H2	Type	Psia	T	Mth vap	H2 vap	Mth liq	H2 liq
<b>Methane and Hydrogen Only</b>											
1% H <sub>2</sub> , C1, 15.5	400	-258	99.00%	1.00%	M/H	15.5	-264.2	75.06	24.94%	99.94%	0.06%
1% H <sub>2</sub> , C1, 16.5	400	-258	98.96%	1.04%	M/H	16.5	-263.6	72.76%	27.24%	99.93%	0.07%
5% H <sub>2</sub> , C1	400	-258	95.00%	5.00%	M/H	16.5	-271.7	48.70%	51.30%	99.85%	0.15%
10% H <sub>2</sub> , C1, 14.5	400	-258	90.00%	10.00%	M/H	14.5	-277.6	40.17%	59.83%	99.83%	0.17%
10% H <sub>2</sub> , C1, 15.5	400	-258	90.00%	10.00%	M/H	15.5	-276.8	39.30%	60.70%	99.82%	0.18%
10% H <sub>2</sub> , C1	400	-258	90.00%	10.00%	M/H	16.5	-276.1	38.47%	61.53%	99.81%	0.19%
20% H <sub>2</sub> , C1	400	-258	80.00%	20.00%	M/H	16.5	-281.4	28.51%	71.49%	99.76%	0.24%
<b>LNG including Methane, Ethane, Propane, Nitrogen and Hydrogen</b>											
1% H <sub>2</sub> , LNG	400	-229	94.30%	1.00%	LNG	16	-258.6	90.13%	7.62%	94.92%	0.02%
2% H <sub>2</sub> , LNG	400	-229	93.30%	2.00%	LNG	16	-260.2	84.04%	13.87%	94.83%	0.04%
3% H <sub>2</sub> , LNG	400	-229	92.30%	3.00%	LNG	16	-261.6	78.80%	19.16%	94.75%	0.06%
4% H <sub>2</sub> , LNG	400	-229	91.30%	4.00%	LNG	16	-262.8	74.42%	23.74%	94.66%	0.07%
5% H <sub>2</sub> , LNG	400	-229	90.30%	5.00%	LNG	16	-263.9	70.81%	27.46%	94.57%	0.80%
6% H <sub>2</sub> , LNG	400	-229	89.30%	6.00%	LNG	16	-264.8	67.73%	30.64%	94.47%	0.08%
7% H <sub>2</sub> , LNG	400	-229	88.30%	7.00%	LNG	16	-265.7	65.00%	33.45%	94.38%	0.11%
8% H <sub>2</sub> , LNG	400	-229	87.30%	8.00%	LNG	16	-266.4	62.57%	35.96%	94.28%	0.12%
9% H <sub>2</sub> , LNG	400	-229	86.30%	9.00%	LNG	16	-267.2	60.37%	38.23%	94.18%	0.12%
10% H <sub>2</sub> , LNG	400	-229	85.30%	10.00%	LNG	16	-267.8	58.37%	40.28%	94.08%	0.13%
20% H <sub>2</sub> , LNG	400	-229	75.30%	20.00%	LNG	16	-272.5	46.12%	52.92%	94.11%	0.19%



# SUMMARY OF FINDINGS

- A full 1 BCF tank contains  $\sim 42,500,000$  lbm of LM
- Amount of heat needed to lower  $42,500,000$  lbm of LM  $5^{\circ}\text{F}$  would be  $177,000,000$  Btu ( $C_p = 0.835$  Btu/lbm  $^{\circ}\text{F}$ ).
- All the cooling is from the evaporation of methane forced by the lower vapor pressure of methane.
  - Fick's Law, Daltons Law, LaChatelier's principle
- The amount of heat leak that comes into the tank each day is approximately  $42,500,000$  lbm  $\times 0.005 \times 218$  Btu/lbm =  $4,600,000$  Btu/day.
  - After a long liquefaction run it would take  $\sim 50$  days for BOG to normalize  $177,000,000$  Btu/ $4,600,000$  Btu/day = 40 -50 days
- The amount of cooling provided by a  $5,000,000$  scfd liquefier is:
  - $5,000,000$  scfd  $\times .04246$  lbm/scf  $\times 356$  Btu/lbm =  $\sim 75,800,000$  Btu of heat removed per day.

# CHALLENGING OPPORTUNITIES IDENTIFIED DURING THE PROJECT

- Can a laboratory or in-field experiment be made to validate these software outputs?
- Further analysis of the materials of construction impacts of hydrogen in legacy liquefaction facilities and assessing material failure risks with feedstock containing hydrogen.
- What equation of state thermodynamic modeling software is available to examine natural gas/hydrogen blends? (non-convergence/accuracy of REFPROP and HYSYS)
- What is the preferred management method of the off-gas that contains hydrogen?





# THANK YOU

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